



Robot Motion Planning for Multiple Moving Objects Interception with constant acceleration

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Abstract: This paper presents a novel approach to on-line, robot-motion planning for multiple moving-objects interception with constant acceleration. The position, velocity and acceleration of the free particles are used as kinematics information. This information is used to obtain the multiple interception trajectory. The polynomial interpolation technique is implemented in a 2D robot with to follow the follower-trajectory generated. The implementation of the proposed technique is illustrated via a simulation example. It consists of the 2D multiple interception of two objects moving along a well-known parabolic trajectory via a robot interceptor.

Keywords: Robot planning, multiple interception, trajectory.

Introduction

The problem addressed in this paper is the multiple interception of two or more free particles moving with constant acceleration. A slow-maneuvering target moves on a continuous path with a relatively constant acceleration. The state (position and velocity) of the objects as a function of time is obtained through a vision system. The moving objects are assumed to stay within the robot's workspace for a limited time.

The multiple interception task is defined as "approaching to multiple moving objects while matching their locations and velocities in the shortest possible time." [1]. Prediction, planning, and execution (PPE) methods are well suited for intercepting objects traveling along predictable trajectories, when using PPE technique, the robot is directly sent to an anticipated rendezvous point on the target's predicted trajectory [4-7].

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Problem definition: The n particles: TFL_1 (Trajectory of the Free Particle 1), TFL_2 (Trajectory of the Free Particle 2), TFL_n (Trajectory of the Free Particle n) and TFP (Trajectory of the Following Particle). TFL_i , $i=1,\dots,n$ describe well-known trajectories. In time $t=t_0=0$ s, begin their motion from the initial position (x_1, y_1, z_1) , $(x_2, y_2, z_2), \dots, (x_n, y_n, z_n)$, respectively. TFP is a trajectory to be calculated mathematically. TFP begins its motion at the initial position (ax, ay, az) in the delayed time $t=t_1$ where $t_0 < t_1 \leq T^*$. T^* is a bounded time obtained from the limit job space of the robot [2-3].

The function TFP have to intercept TFL_1 in the instant of time t_2 and to equal the direction of its trajectory in the interval of time $\Delta t_2 = t_3 - t_2$, then, have to intercept TFL_2 in the instant of time t_4 and to equal the direction of its trajectory in the interval of time $\Delta t_4 = t_5 - t_4$, thus, successively until intercepting to TFL_n equal the direction of its trajectory in the interval of time $\Delta t_n = t_{n+1} - t_n$. see fig (1).

Methodology of multiple 3D interception of well-known trajectories: A methodology to solve the problem to calculate mathematically the following-trajectory TFP that intercepts the trajectories described by TFL_i , $i=1,\dots,n$ in the defined times t_2, t_4, \dots, t_n , is presented.

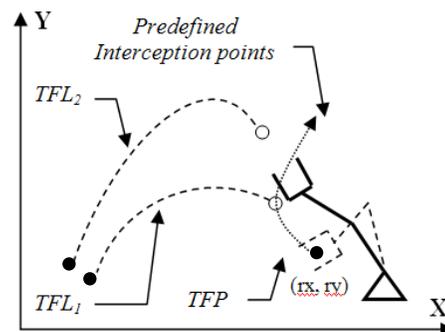


Fig. 1. Trajectories TFL_1 , TFL_2 and TFP .



The function TFL_i (Trajectory of the Free Particle i): The n trajectories generated by the particles TFL_i , $i=1, \dots, n$ can be represented in the parametric form, being t the parameter [2-3], see (1).

$$TFL_i = (X_i(t), Y_i(t), Z_i(t))^T, \quad i=1, \dots, n \quad (1)$$

The components of eq.(1): $X_1(t), Y_1(t), Z_1(t), \dots, X_n(t), Y_n(t), Z_n(t)$ are functions formed with the next form with constant acceleration. See (2).

$$TFL_n \begin{cases} X_n(t) = x_{0n} + V_{x0n}t + \frac{1}{2}a_{xn}t \\ Y_n(t) = y_{0n} + V_{y0n}t + \frac{1}{2}a_{yn}t \\ Z_n(t) = z_{0n} + V_{z0n}t + \frac{1}{2}a_{zn}t \end{cases} \quad (2)$$

Where x_{0n}, y_{0n} and z_{0n} are the initial position of the n^{th} particle. In the same way, V_{x0n}, V_{y0n} and V_{z0n} are the initial velocity. The constant acceleration components are: a_{xn}, a_{yn}, a_{zn} . The acceleration governs the trajectory topology of the particle. This information can be obtained using a vision system.

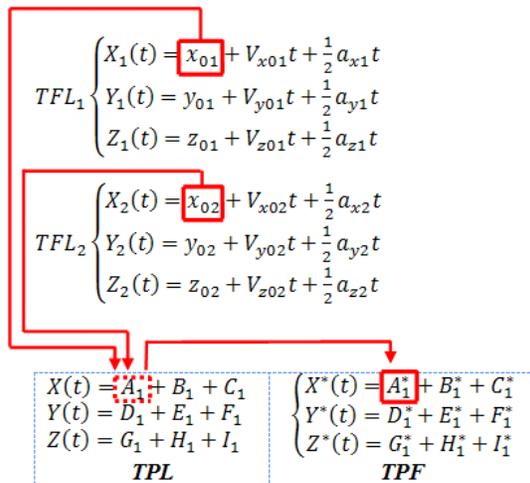


Fig. 2. Grouping the terms of the function TFL.

The fig. 2, shows the way how can represent the components in the correspondent term in the function TFL. In the same way can be obtained for the velocity and acceleration. In the compact form: see (3).

$$TFL_i \begin{cases} X_i(t) = \sum_{j=1}^k T_{x_{ij}}(t) \\ Y_i(t) = \sum_{j=1}^l T_{y_{ij}}(t) \\ Z_i(t) = \sum_{j=1}^m T_{z_{ij}}(t) \end{cases} \quad (3)$$

Where: k, l and m are the total number of terms of the functions $X_i(t), Y_i(t)$ and $Z_i(t)$, respectively.

The function TFP (Trajectory of the Following-Particle): To generate the following-trajectory TFP the following functions are proposed, position, velocity and acceleration, respectively, see (4):

$$\begin{aligned} TFP &= (X^*(t), Y^*(t), Z^*(t)) \\ T\dot{F}P &= (\dot{X}^*(t), \dot{Y}^*(t), \dot{Z}^*(t)) \\ T\ddot{F}P &= (\ddot{X}^*(t), \ddot{Y}^*(t), \ddot{Z}^*(t)) \end{aligned} \quad (4)$$

The components of the following-function TFP can be expressed, as (5), (6) and (7): Could be represented as follows:

$$TFP = \begin{cases} X^*(t) = A_1 + B_1 + C_1 \\ Y^*(t) = D_1 + E_1 + F_1 \\ Z^*(t) = G_1 + H_1 + I_1 \end{cases} \quad (5)$$

$$T\dot{F}P = \begin{cases} \dot{X}^*(t) = \dot{A}_1 + \dot{B}_1 + \dot{C}_1 \\ \dot{Y}^*(t) = \dot{D}_1 + \dot{E}_1 + \dot{F}_1 \\ \dot{Z}^*(t) = \dot{G}_1 + \dot{H}_1 + \dot{I}_1 \end{cases} \quad (6)$$

$$T\ddot{F}P = \begin{cases} \ddot{X}^*(t) = \ddot{A}_1 + \ddot{B}_1 + \ddot{C}_1 \\ \ddot{Y}^*(t) = \ddot{D}_1 + \ddot{E}_1 + \ddot{F}_1 \\ \ddot{Z}^*(t) = \ddot{G}_1 + \ddot{H}_1 + \ddot{I}_1 \end{cases} \quad (7)$$

Representating in the compact form.

$$\begin{aligned} X^*(t) &= \sum_{j=1}^k T_{x_j^*}(t), \\ Y^*(t) &= \sum_{j=1}^l T_{y_j^*}(t), \\ Z^*(t) &= \sum_{j=1}^m T_{z_j^*}(t) \end{aligned} \quad (8)$$



Estimating the terms $Tx_j^*(t), Ty_j^*(t), Tz_j^*(t)$: For each term $Tx_{ij}(t), Ty_{ij}(t)$ and $Tz_{ij}(t)$ of the functions $X_i(t), Y_i(t)$ and $Z_i(t)$ shown in (2), the functions $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$ are proposed, respectively, that intercepts each one of the terms.

In other words, it is necessary to know the kinematics information of each term $Tx_{ij}(t), Ty_{ij}(t)$ and $Tz_{ij}(t)$. With this information we generate the functions: $X_i(t), Y_i(t)$ and $Z_i(t)$ of the trajectories described by free particles $TFLi, i=1, \dots, n$ in order to calculate the terms $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$ they have the form of the following-trajectory TFP . Without loss of generality, as example to illustrate the methodology we only develop $Tx_j^*(t)$ with $j=0$, that is; $Tx_0^*(t)$, the information of $Tx_{ij}(t), i=0, \dots, n$ is used, that is, the terms: $Tx_{00}(t), Tx_{10}(t), \dots, Tx_{n0}(t)$, are expressed in (2) and illustrated in fig. 3.

We take the first term $Tx_{i0}(t), i=0, \dots, n$ of each function $X_i(t), i=0, \dots, n$, the terms are shown in fig. 3.

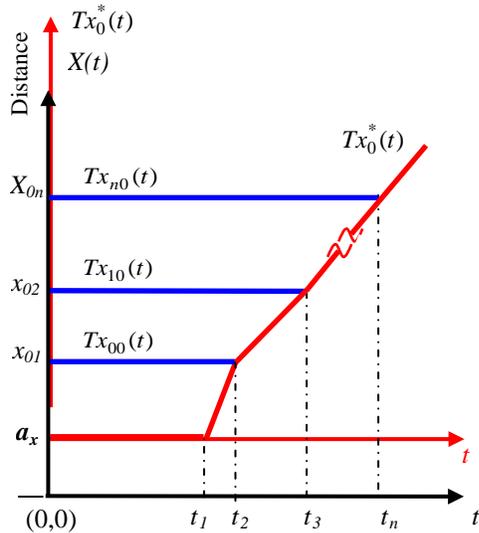


Fig.3 Estimation of the function $Tx_0^*(t)$ and $\Delta t_2=t_3-t_2$ and $\Delta t_4=t_5-t_4$ intervals of time.

We can observe that $Tx_0^*(t)$ intercepts $Tx_{00}(t)$ in the time t_2 , and to equal the direction of its trajectory in

the interval of time $\Delta t_2=t_3-t_2$. Then, it intercepts $Tx_{10}(t)$ in the time t_4 , and to equal the direction of its trajectory in the interval of time $\Delta t_4=t_5-t_4$.

Finally, it intercepts to $Tx_{n0}(t)$ in the time t_n and to equal the direction of its trajectory in the interval of time $\Delta t_n=t_{n+1}-t_n$. To calculate $Ty_0^*(t)$ is also required to know the functions $Ty_{00}(t), Ty_{10}(t), \dots, Ty_{n0}(t)$, which are the terms of $Y_i(t)$. $Tz_0^*(t)$ can be obtained in the same way. In the table 1, the information of the terms: $Tx_{ij}(t), Ty_{ij}(t)$ and $Tz_{ij}(t)$ necessary to calculate $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$ respectively, are presented.

Table 1. Information to estimate $Tx_j^*(t)$		
j	$Tx_j^*(t)$	Terms: $Tx_{ij}(t), i=0, \dots, n$
0	$Tx_0^*(t)$	$Tx_{00}(t), Tx_{10}(t), Tx_{20}(t), \dots, Tx_{n0}(t)$
1	$Tx_1^*(t)$	$Tx_{01}(t), Tx_{11}(t), Tx_{21}(t), \dots, Tx_{n1}(t)$
2	$Tx_2^*(t)$	$Tx_{02}(t), Tx_{12}(t), Tx_{22}(t), \dots, Tx_{n2}(t)$
..	
k	$Tx_k^*(t)$	$Tx_{0k}(t), Tx_{1k}(t), Tx_{2k}(t), \dots, Tx_{nk}(t)$

Form of the functions $Tx_j^*(t), Ty_j^*(t), Tz_j^*(t)$. We propose the functions $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$ be of the polynomial type:

$$\begin{aligned}
 Tx_j^*(t) &= \alpha_0^x + \alpha_1^x t + \alpha_2^x t^2 + \dots + \alpha_{2n}^x t^{2n}, & j=0, \dots, k \\
 Ty_l^*(t) &= \alpha_0^y + \alpha_1^y t + \alpha_2^y t^2 + \dots + \alpha_{2n}^y t^{2n}, & j=0, \dots, l \\
 Tz_m^*(t) &= \alpha_0^z + \alpha_1^z t + \alpha_2^z t^2 + \dots + \alpha_{2n}^z t^{2n}, & j=0, \dots, m
 \end{aligned}
 \tag{9}$$

Developing the subindex j , the equations (7), take the form of (8):

$$\begin{aligned}
 Tx_k^*(t) &= \zeta_0^x + \zeta_1^x t + \zeta_2^x t^2 + \dots + \zeta_{2n}^x t^{2n}, \\
 Ty_l^*(t) &= \zeta_0^y + \zeta_1^y t + \zeta_2^y t^2 + \dots + \zeta_{2n}^y t^{2n}, \\
 Tz_m^*(t) &= \zeta_0^z + \zeta_1^z t + \zeta_2^z t^2 + \dots + \zeta_{2n}^z t^{2n}
 \end{aligned}
 \tag{10}$$

Denoting that the coefficients proposed should be different for each function $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$.



Estimate of the coefficients $\alpha_i^x, \alpha_i^y, \alpha_i^z, \beta_i^x, \beta_i^y, \beta_i^z, \dots, \zeta_i^x, \zeta_i^y, \zeta_i^z, i=0, \dots, n+2$. A polynomial type of equations system are proposed to calculate the coefficients of each function $Tx_j^*(t), Ty_j^*(t)$ and $Tz_j^*(t)$ of (9). The values: a_x, a_y and a_z represent the initial position of the trajectory TFP , they are included in the system of equations (9), (10) and (11).

To obtain the function $Tx_j^*(t)$ with $j=0$, we have:

$$\begin{aligned} \alpha_0^x + \alpha_1^x t_1 + \alpha_2^x t_1^2 + \dots + \alpha_{2n}^x t_1^{2n} &= ax \\ \alpha_0^x + \alpha_1^x t_{2n} + \dots + \alpha_{2n}^x t_{2n}^{2n} &= Tx_{n0}(t_{2n}) \\ \alpha_0^x + \alpha_1^x t_{2n+1} + \dots + \alpha_{2n}^x t_{2n+1}^{2n} &= Tx_{n0}(t_{2n+1}) \end{aligned} \quad (11)$$

To obtain the function $Ty_j^*(t)$ with $j=0$, we have:

$$\begin{aligned} \alpha_0^y + \alpha_1^y t_1 + \alpha_2^y t_1^2 + \dots + \alpha_{2n}^y t_1^{2n} &= ay \\ \alpha_0^y + \alpha_1^y t_{2n} + \dots + \alpha_{2n}^y t_{2n}^{2n} &= Ty_{n0}(t_{2n}) \\ \alpha_0^y + \alpha_1^y t_{2n+1} + \dots + \alpha_{2n}^y t_{2n+1}^{2n} &= Ty_{n0}(t_{2n+1}) \end{aligned} \quad (12)$$

And to obtain $Tz_j^*(t)$ with $j=0$, we have:

$$\begin{aligned} \alpha_0^z + \alpha_1^z t_1 + \alpha_2^z t_1^2 + \dots + \alpha_{2n}^z t_1^{2n} &= az \\ \alpha_0^z + \alpha_1^z t_{2n} + \dots + \alpha_{2n}^z t_{2n}^{2n} &= Tz_{n0}(t_{2n}) \\ \alpha_0^z + \alpha_1^z t_{2n+1} + \dots + \alpha_{2n}^z t_{2n+1}^{2n} &= Tz_{n0}(t_{2n+1}) \end{aligned} \quad (13)$$

An Example of Application. Two objects are moving in parabolic trajectory in the bi-dimensional space as shown in fig. 2 with the following data: TFL_1 , Initial position: $X_{01}=0.0m, Y_{01}=5.0m, Z_{10}=0.0m, V_{x01}=8.0m/s, V_{y01}=40.0m/s$, Interception time 1: $t_2=6.0s$, Interval of time $\Delta t_2=0.01s$, time to catch $t_3=10.1s$. TFL_2 , Initial position: $X_{02}=0.0m, Y_{02}=10.0m, Z_{20}=0.0m, V_{x02}=6.5m/s, V_{y02}=6.5m/s$, Interception time 2. The delay time is: $t_1=0.5s$. the acceleration terms are: $a_{x1}=a_{x2}=a_{z1}=a_{z2}=0$ and $a_{y1}=a_{y2}=g=9.81\text{ m/s}$, the initial position of the following-trajectory: $a_x=20m, a_y=30m$. [8-9]. To design the following trajectory TFP to intercept the two objects using the defined intervals of time to avoid the impact. The integration step is $\Delta t=0.1\text{ s}$. The delayed time: $t_l=0.5s$. The initial position of TFP is $(a_x=r_x, a_y=r_y, 0)$. Using the proposed methodology above described.

Solution of the example: Applying the steps of the methodology of multiple interception, we have:

The trajectories $TFL_i, i=1,2$. The parabolic trajectories can be mathematically described as follows:

$$TFL_1 \begin{cases} X_1(t) = x_{01} + V_{x01}t + \frac{1}{2}a_{x1}t \\ Y_1(t) = y_{01} + V_{y01}t + \frac{1}{2}a_{y1}t \\ Z_1(t) = 0 \end{cases} \quad (14)$$

$$TFL_2 \begin{cases} X_2(t) = x_{02} + V_{x02}t + \frac{1}{2}a_{x2}t \\ Y_2(t) = y_{02} + V_{y02}t + \frac{1}{2}a_{y2}t \\ Z_2(t) = 0 \end{cases} \quad (15)$$

The function TFP . The form of the function TFP , include the initial position of TFL_1 and TFL_2 . To calculate the term A_1^* of the term of the component $X(t)$, see (16) a equation system of 9×9 , is proposed to find the unknown variables:

$\alpha_0, \alpha_1, \alpha_2, \alpha_3, \alpha_4, \alpha_5, \alpha_6, \alpha_7, \alpha_8$. The number of incognits must be equal to the number of the terms of the TFL_i function.

equation	A_1	B_1	C_1
$f_1 = \alpha_0 + \sum_{i=0}^{n=8} \alpha_i t_1 =$	r_x		
$\dot{f}_1 =$	0		
$\ddot{f}_1 =$	0		
$f_2 = \alpha_0 + \sum_{i=0}^{n=8} \alpha_i t_2 =$	x_{01}		
$\dot{f}_2 =$	0		
$\ddot{f}_2 =$	0		
$f_3 = \alpha_0 + \sum_{i=0}^{n=8} \alpha_i t_3 =$	x_{02}		
$\dot{f}_3 =$	0		
$\ddot{f}_3 =$	0		

Solving the system equation mentioned above, we obtain the unknown variables: The component A_1^* of the follower-trajectory: TFP are:

$$\begin{aligned} A_1^* &= \\ \alpha_0 + \alpha_1 t + \alpha_2 t^2 + \alpha_3 t^3 + \alpha_4 t^4 + \alpha_5 t^5 + \alpha_6 t^6 + \alpha_7 t^7 + \alpha_8 t^8 \\ A_1^* &= \\ \alpha_1 + 2\alpha_2 t + 3\alpha_3 t^2 + 4\alpha_4 t^3 + 5\alpha_5 t^4 + 6\alpha_6 t^5 + 7\alpha_7 t^6 + 8\alpha_8 t^7 \\ \dot{A}_1^* &= \\ 2\alpha_2 + 6\alpha_3 t + 12\alpha_4 t^2 + 20\alpha_5 t^3 + 30\alpha_6 t^4 + 42\alpha_7 t^5 + 56\alpha_8 t^6 \end{aligned} \quad (16)$$



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A(t)

f1 = a0 + a1 t1 + a2 t1^2 + a3 t1^3 + a4 t1^4 + a5 t1^5 + a6 t1^6 + a7 t1^7 + a8 t1^8 == xx
f2 = 0 + a1 + 2 a2 t1 + 3 a3 t1^2 + 4 a4 t1^3 + 5 a5 t1^4 + 6 a6 t1^5 + 7 a7 t1^6 + 8 a8 t1^7 == 0
f3 = 0 + 0 + 2 a2 + 6 a3 t1 + 12 a4 t1^2 + 20 a5 t1^3 + 30 a6 t1^4 + 42 a7 t1^5 + 56 a8 t1^6 == 0

f4 = a0 + a1 t2 + a2 t2^2 + a3 t2^3 + a4 t2^4 + a5 t2^5 + a6 t2^6 + a7 t2^7 + a8 t2^8 == x01
f5 = 0 + a1 + 2 a2 t2 + 3 a3 t2^2 + 4 a4 t2^3 + 5 a5 t2^4 + 6 a6 t2^5 + 7 a7 t2^6 + 8 a8 t2^7 == 0
f6 = 0 + 0 + 2 a2 + 6 a3 t2 + 12 a4 t2^2 + 20 a5 t2^3 + 30 a6 t2^4 + 42 a7 t2^5 + 56 a8 t2^6 == 0

f7 = a0 + a1 t3 + a2 t3^2 + a3 t3^3 + a4 t3^4 + a5 t3^5 + a6 t3^6 + a7 t3^7 + a8 t3^8 == x02
f8 = 0 + a1 + 2 a2 t3 + 3 a3 t3^2 + 4 a4 t3^3 + 5 a5 t3^4 + 6 a6 t3^5 + 7 a7 t3^6 + 8 a8 t3^7 == 0
f9 = 0 + 0 + 2 a2 + 6 a3 t3 + 12 a4 t3^2 + 20 a5 t3^3 + 30 a6 t3^4 + 42 a7 t3^5 + 56 a8 t3^6 == 0

Sol = Solve[{f1, f2, f3, f4, f5, f6, f7, f8, f9}, {a0, a1, a2, a3, a4, a5, a6, a7, a8}];
s = {a0, a1, a2, a3, a4, a5, a6, a7, a8} /. Sol;
a0 = s[[1]][[1]];
a1 = s[[1]][[2]];
a2 = s[[1]][[3]];
a3 = s[[1]][[4]];
a4 = s[[1]][[5]];
a5 = s[[1]][[6]];
a6 = s[[1]][[7]];
a7 = s[[1]][[8]];
a8 = s[[1]][[9]];

A1 = FullSimplify[a0 + a1 t + a2 t^2 + a3 t^3 + a4 t^4 + a5 t^5 + a6 t^6 + a7 t^7 + a8 t^8]
A1P = FullSimplify[a1 + 2 a2 t + 3 a3 t^2 + 4 a4 t^3 + 5 a5 t^4 + 6 a6 t^5 + 7 a7 t^6 + 8 a8 t^7]
A1PP = FullSimplify[2 a2 + 6 a3 t + 12 a4 t^2 + 20 a5 t^3 + 30 a6 t^4 + 42 a7 t^5 + 56 a8 t^6]

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Fig.4 Programming code to solve the equation system, using the mathematica® 5.0 software.

Then, we have the polynomials components:

$$\begin{aligned}
 TPL &= \begin{cases} X^*(t) = A_1^* + B_1^* + C_1^* \\ Y^*(t) = D_1^* + E_1^* + F_1^* \\ Z^*(t) = G_1^* + H_1^* + I_1^* \end{cases} \\
 T\dot{P}L &= \begin{cases} \dot{X}^*(t) = \dot{A}_1^* + \dot{B}_1^* + \dot{C}_1^* \\ \dot{Y}^*(t) = \dot{D}_1^* + \dot{E}_1^* + \dot{F}_1^* \\ \dot{Z}^*(t) = \dot{G}_1^* + \dot{H}_1^* + \dot{I}_1^* \end{cases} \quad (17) \\
 T\ddot{P}L &= \begin{cases} \ddot{X}^*(t) = \ddot{A}_1^* + \ddot{B}_1^* + \ddot{C}_1^* \\ \ddot{Y}^*(t) = \ddot{D}_1^* + \ddot{E}_1^* + \ddot{F}_1^* \\ \ddot{Z}^*(t) = \ddot{G}_1^* + \ddot{H}_1^* + \ddot{I}_1^* \end{cases}
 \end{aligned}$$

Using the similar technique above mentioned for each other terms of the functions, see (17).

Numerical Results: Finally, substituting the coefficients values in (18) and adding in (17), we obtain

the components of the trajectory *TFP*, which is shown in fig.3 and 4.

$$\begin{aligned}
 X^*(t) &= 19.5 + 3.6t - 8.7t^2 - 8.9t^3 - 3.7t^4 + 0.8t^5 \\
 &\quad - 0.09t^6 + 0.005t^7 - 0.00013t^8 \\
 Y^*(t) &= 31.5 - 10.6t + 27.02t^2 - 31.1t^3 + 16.1t^4 \\
 &\quad - 4.0t^5 + 0.5t^6 - 0.03t^7 \\
 &\quad - 0.0008t^8 \\
 \dot{X}^*(t) &= 3.66 - 17.5t + 26.81t^2 - 14.92t^3 + 4.03t^4 \\
 &\quad - 0.57t^5 + 0.04t^6 - 0.001t^7 \\
 \dot{Y}^*(t) &= -10.6 + 54.0t - 93.3t^2 + 64.6t^3 - 20.1t^4 \\
 &\quad + 3.08t^5 - 0.23t^6 + 0.006t^7 \\
 \ddot{X}^*(t) &= -17.46 + 53.62t - 44.76t^2 + 16.13t^3 \\
 &\quad - 2.83t^4 + 0.23t^5 - 0.008t^6 \\
 \ddot{Y}^*(t) &= -6.26 - 6.61t + 53.32t^2 - 33.89t^3 \\
 &\quad + 7.83t^4 - 0.77t^5 + 0.03t^6
 \end{aligned} \quad (18)$$

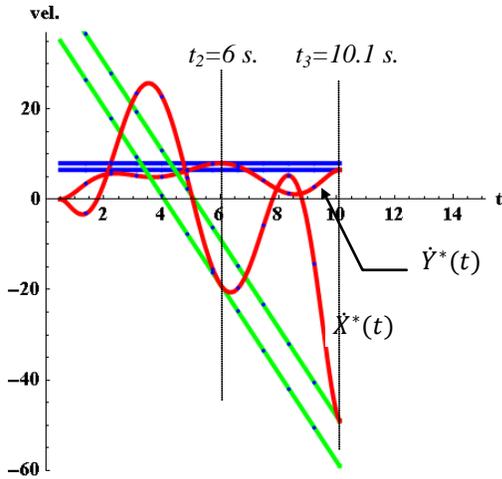


Fig. 5. Space-time phenomenon interception. Velocity.

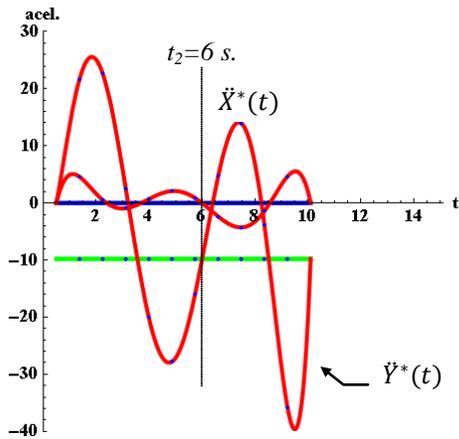


Fig. 6. Space-time phenomenon interception. Acceleration.

The Fig. 5, 6 and 7, shows the x-y-t graphics of the two TFL_1 and TFL_2 trajectories and the follower-trajectory TFP . The speed of the trajectory TFP is equal with respect to the trajectories TFL_1 y TFL_2 in the intervals of time Δt_2 , Δt_4 , also the direction of the trajectory TFP attempts to equal the direction of the TFL 's in the intervals of time Δt 's.

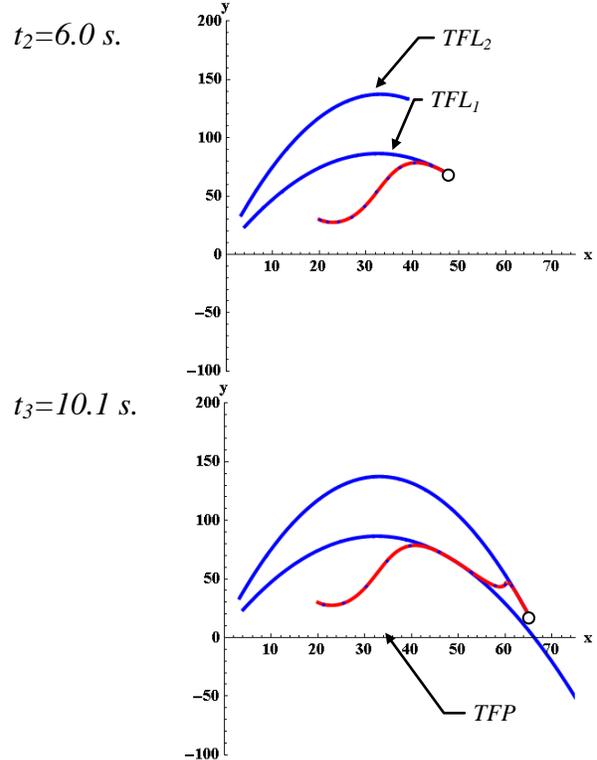


Fig. 7. The physical phenomenon of interception. Position.

Conclusions

This paper presented a novel approach to on-line, robot-motion planning for moving-objects multiple 3D object interception using a polynomial interpolation approach.

In the intervals of time the follower trajectory attempts to equal the direction of the trajectories TFL 's, allowing the robot captures the objects without impact. The implementation of the proposed methodology has been illustrated via simulation examples; here only one of them was presented. It has been clearly shown that the methodology proposed herein yields results favorable over the conventional tracking one object methods.



References

- [1] Mehran Mehrandezh, *et al*, "Robotic Interception of Moving Objects Using an Augmented Ideal Proportional Navigation Guidance Technique", *IEEE Transactions on Systems, Man and Cybernetics-part a: Systems and Humans*, vol. 30, No. 3, pp.~238-250, May. 2000.
- [2] J. A. Flores Campos, *et al*, "Robot Trajectory Planning for Multiple 2D Moving Objects Interception: a Functional Approach," *cerma*, pp. 77-82, Electronics, Robotics and Automotive Mechanics Conference (CERMA'06), 2006.
- [3] J. A. Flores Campos, J. A. Rosas Flores, C. Palacios Montúfar, "Robot Interceptor an Experimental Approach", *Fourth Congress of Electronics, Robotics and Automotive Mechanics*, pp.476-481, 2007
- [4] T. H. Park and B. H. Lee, "An approach to robot analysis and planning for conveyor tracking," *IEEE, Trans. Syst., Man, Cybern.*, vol. 22, pp. 378-384, 1992.
- [5] G. C. Buttazzo, B. Allotta and F. P. Fanizza, "Mousebuster: A Robot for Real-Time Catching," *IEEE Control Systems*, vol. 14, No. 1, pp. 49-56, 1994.
- [6] N. P. Papanikolopoulos, P.K. Khosla, and T. Kanade, "Visual Tracking of a moving Target by a Camera Mounted on a Robot: A Combination of Control and Vision," *IEEE, Transactions on Robotics and Automation*, vol. 9, No.1, pp. 14-35, 1993.
- [7] H. R. Piccardo and G. Hondered, "A new approach to on-line path planning and generation for robots in nonstatic environment," *J. Robot. Automat. Syst.*, pp. 187-201, 1991.
- [8] Won Hong, "Robotic Catching and Manipulation Using Active Vision", *Bachelor of Science, University of California at Berkeley, Certificate by Jean-Jacques E. Slotine*, pp, 65, 1992.
- [9] H. Isil Bozma, Hulya Yalcin, "Visual processing and classification of items on a moving conveyor: a selective perception approach", *Robotics and Computer Integrated Manufacturing*, Vol. 18, pp.~125-133, 2002.

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